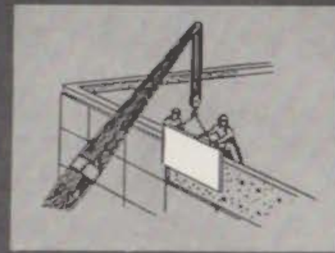
Texas Architect

NOVEMBER, 1961



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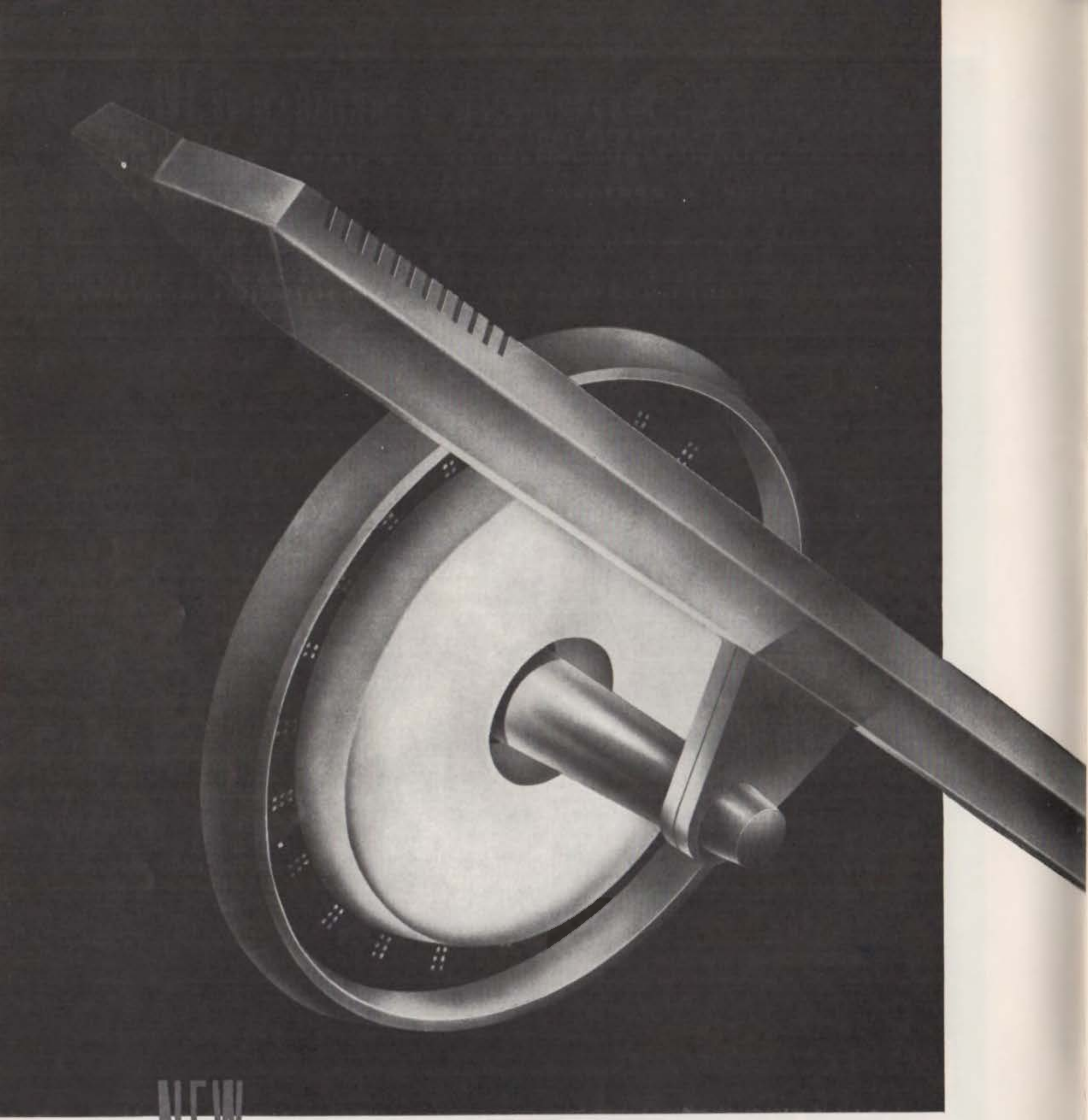

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THE TEXAS ARCHITECT

Vol. 12 — November, 1961 — Number 9

Official Publication of

THE TEXAS SOCIETY OF ARCHITECTS

The Texas Regional Organization of The American Institute of Architects

Don Edward Legge, A.I.A., Editor
John G. Flowers, Jr., Managing Editor

327 Perry-Brooks Building, Austin, Texas

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TEXAS ARCHITECTURAL FOUNDATION
327 Perry - Brooks Building, Austin, Texas

COVER

The striking photo on this month's cover presents the Massachusetts Mutual Insurance Co. office building in El Paso, an outstanding example in the use of decorative units. (Architects: Garland & Hilles). It is also a winner of TCMA's annual award in the commercial construction division.

The President's Letter

By
L. W. "SKEET" PITTS
President
Texas Society of Architects

Education has been called "the cheapest defense of nations." Today it is a magic word. Many talk of ways to improve our systems in America—many are doing something about it. A good education is more important than ever.

The Texas Society of Architects is dedicating its 1961 Annual Convention to Architectural Education. The Texas Architectural Foundation is diligently seeking funds that can be used to improve the teaching of architecture and to assist the students in advancing their education. The Association of Collegiate Schools of Architecture and the American Institute of Architects have jointly made a real contribution with their summer seminars for young teachers and potential teachers. We can be proud of these fine efforts.

No one can serve on our National Committee on Education—take his turn on a College Accreditation Inspection Team—or work with young architects in the office and fail to appreciate the value of top quality in the teaching profession. A department or school of architecture mirrors the capability of its director and his staff. In Texas, we are blessed with a number of dedicated and talented architects who are making it their business to train our future practitioners. We should be grateful to these men—we should make our appreciation known and we should offer our fullest cooperation towards a program for building greater remuneration and even more stature for this high calling.

The desire to teach and the capacity to teach must be expanded. One step in this direction is support of arrangements for our teachers of architecture to enrich their knowledge by actual practice, provided such activity does not interfere with their prime responsibility to their college or university. A successful teacher must learn more than he can teach. It is disturbing to find a few persons who do not grasp the importance of expanding a teachers horizon through actual practice concurrent with teaching. How could a surgeon teach without operating?

We are experiencing great educational movements in our country today — new teaching techniques — accelerated programs for the gifted—more graduate work—adults returning for more education in advanced and refined areas. To support these important movements we must recruit and maintain a larger staff of qualified teachers.

Emerson has said "The secret of education lies in respecting the pupil"—surely the secret also lies in respecting the educator.

Faithfully yours,

"Skeet" Pitts

L. W. "Skeet" Pitts

22nd Annual

CONVENTION

Texas Society of Architects

CONVENTION PROGRAM

November 8, 1961

8:30 a.m.	Golfers' Breakfast—River Crest Country Club
9:30 a.m.	Texas Quarries' Golf Tournament
10:00 a.m.	Registration, Mezzanine Floor, Texas
3:30 p.m.	TSA Study Committee on organization of AIA
4:00 p.m.	Chapter Officers Conclave—Convention Meeting Room, Mezzanine Floor
4:30 p.m.	TSA Executive Committee Meeting
5:00 p.m.	Visit Educational Exhibits and Hospitality Room, Mezzanine Floor
6:00 p.m.	Close Registration
7:30 p.m.	Transportation to Casa Manana Theatre at 8th Street entrance of Texas Hotel
8:15 p.m.	Casa Manana world premiere of "Take Me For An Angel"

November 9, 1961

8:00 a.m.	Acme Brick Breakfast—Fort Worth Club
9:00 a.m.	Registration
9:30 a.m.	Opening Business Session—Robert P. Woltz, Jr., Convention Chairman, presiding Invocation—Dr. G. Alfred Brown, District Superintendent of Methodist Churches Hon. John Justin, Mayor of Fort Worth, Greetings Thaddeus P. Harden, Jr., President, Fort Worth Chapter, Greetings L. W. Pitts, F.A.I.A., President's Report Reginald Roberts, A.I.A., Regional Director's Report TSA Business Session, L. W. Pitts, F.A.I.A., presiding

* * * *

11:00 p.m.	Ladies Visit the Amon Carter Museum of Western Art
12:00 noon	Ladies Sherry Party—Shady Oaks Country Club
12:45 p.m.	Ladies Luncheon and Style Show—Shady Oaks Country Club

* * * *

11:30 a.m.	Keynote Address "Education For The Free World"—Dr. John Ely Burchard, Dean of the School of Humanities, M.I.T.
12:15 p.m.	Architects' and Exhibitors' Luncheon, Crystal Ballroom, Texas Hotel
1:30 p.m.	Visit Educational Exhibits and Hospitality Room, Mezzanine Floor
2:30 p.m.	First Seminar Session, Philip D. Creer, F.A.I.A., presiding

4:30 p.m.	Visit Educational Exhibits and Hospitality Room, Mezzanine Floor
5:30 p.m.	Close Ticket Booth
6:30 p.m.	Producers' Council Cocktail Party, Junior Ballroom, Texas Hotel
7:30 p.m.	President's Banquet and Ball, Crystal Ballroom, Texas Hotel

November 10, 1961

8:00 a.m.	Committee Breakfast Meetings Insurance Committee "Early Risers" Breakfast Public Affairs and Public Relations Joint Committee Meeting Preservation of Historic Buildings Committee Office Practice Committee Hospitals and Health Committee Texas Architectural Foundation Board of Trustees
8:30 a.m.	Open Ticket Booth
9:00 a.m.	Visit Educational Exhibits and Hospitality Room, Mezzanine Floor
9:30 a.m.	Second Seminar Session, Philip D. Creer, F.A.I.A., presiding
12:00 noon	Awards Luncheon–Crystal Ballroom, Texas Hotel
2:00 p.m.	Visit Educational Exhibits and Hospitality Room
2:30 p.m.	Closing Business Session, Convention Meeting Room, L. W. Pitts, F.A.I.A., presiding
4:30 p.m.	Post Convention Board Meeting–Santa Gurtrudis Room, Texas Hotel, Harold E. Calhoun, F.A.I.A., presiding
4:30 p.m.	Close Ticket Booth
6:30 p.m.	Transportation to Pioneer Palace at 8th Street entrance of Texas Hotel to "Texas Under Six Flags" Costume Party

CONVENTION COMMITTEE CHAIRMEN

Robert P. Woltz, Jr., Convention Chairman
Edward L. Wilson, F.A.I.A., Committee for Convention Guests
Earl E. Koeppe, Exhibit Booths
Herman G. Cox, President's Dinner and Producers' Council Party
Clyde Hueppelsheuser, Costume Party
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convention program notes

Architectural education is uppermost in the minds of the entire profession in 1961. The challenge to rebuild an entirely new America within the next forty years has focused a penetrating interest on the education of the practitioners who will be called upon to design as much construction in the remaining years of this century as has been built in all of the years of the nations existence.

An unusually distinguished panel of speakers has been invited to examine in depth the whole gamut of architectural education today. The distinguished Dr. John Ely Burchard, Dean of the School of Humanities, M.I.T., will sound the keynote in his address "Education For The Free World."

The probing of the fascinating subject of who should become an architect begins with Dr. Donald G. MacKinnon, Director, Institute of Personality Development and Assessment, University of California. Dr. MacKinnon is a highly regarded specialist in his field and has just recently concluded a several year research project to determine the characteristics of creative people, with emphasis on their selection and guidance into the design professions with a reasonable prediction of success in this field.

The remaining panel speakers, working from the premise that the right people have been guided toward the architectural profession, will commence the examination of the present day college curriculum in architecture and the manifold changes taking place now with a look at future suggestion for further curriculum enrichment. The post-graduate scene, the architect-in-training program, the education of the young practitioner, further education for the older practitioner, education of the public about architects and architecture, and finally, a look at research programs for architecture will be the areas under probing consideration.

Other distinguished panelists will include Walter F. Bogner, F.A.I.A., well known practitioner and Professor in the School of Design at Harvard, who has just completed a year's investigation of architectural schools in Europe; Burnham Kelley, A.I.A., Dean, School of Architecture, Cornell University, who is a planner of note, with a rich experience in planning and practice and a former member of the Research Committee, AIA; Thomas J. Biggs, AIA, practicing architect of Jackson, Mississippi, who is Chairman of the AIA Education Sub-Committee on Architect-in-Training; Mr. Harold Horwitz of the staff of the Building Research Institute in Washington, D. C., who has worked closely with AIA members on research programs, and Mr. Donald Q. Faragher, F.A.I.A., practicing architect of Rochester, New York, Chairman of the AIA Education Committee and Past President of the New York State Association of Architects.

The educational exhibits of new materials, new applications and new products are especially important for all practitioners this year.

The exhibits of the winners of the Texas Architecture—1961 competition and the exhibits of the student award winners are also on display.

But no convention is complete without a gracious and lively social program. Two most unusual events are scheduled for Fort Worth. The world premiere of an American comedy which is Broadway bound and entitled "Take Me For An Angel" is scheduled for Wednesday night at the Casa Manana Theatre. "Texas Under Six Flags" is a gala evening of the sort only Fort Worth can provide in the Pioneer Palace. It is a costume party with a world of built in surprises. Costumes are to reflect one of the six periods of Texas history.

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CONTROL JOINTS and reinforcing concrete masonry units

BY N. ROBERT BATTEN
Executive Secretary
T.C.M.A.

Technical material furnished through the courtesy of Joseph N. Lucas and J. A. Jones, A.A. Wire Products Company, Chicago. Reprints from Concrete Masonry Information Manual, published by TCMA.

Concrete masonry units, as a building material, are increasing rapidly throughout the United States with more than 2¼ billion units being used in all types of construction.

Concrete masonry, just as other construction materials, is subject to expansion and contraction from various causes, some of which are: moisture change, chemical change, temperature change, unequal settlement of the building foundation, high concentrations of applied loads such as roof members, high stresses in masonry at weakened wall sections and localized built-in restraints, such as columns and intersecting walls.

Cracks in masonry walls are, in effect, nothing more than control joints themselves; however, they usually disfigure a wall and need to be repaired.

CONTROL JOINTS

Cracking can be controlled by proper use of control joints. These joints are continuous from the bottom to the top of the masonry wall and are constructed through the entire thickness of the wall.

Since concrete masonry is not a perfectly elastic material, the correct locations for control joints cannot be predicted with mathematical accuracy. Specifying control joints becomes a matter of judgment based on experience and past performance of the concrete masonry units to be used.

Control joints are placed in walls for many reasons, some of which are:

1. At all abrupt changes in wall height
2. In buildings with cast in place concrete foundations which contain joints—the joint should be continued up through the concrete masonry wall.
3. Expansion joints in roof slabs—these joints should also be continued down through the concrete masonry wall.
4. Openings, such as doors and windows – below windows, the joints extend directly below the sides of the openings. Generally, openings less than six feet need only a control joint on one

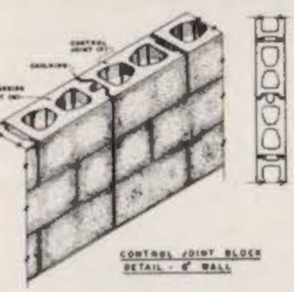
side; wider openings need joints along both sides. Above doors and windows they are offset to the end of the lintels.

5. Where there is an abrupt change in wall thickness at such points as the juncture of a single story wing with a multi-story building or at columns or pilasters.

6. Control joints should be placed in concrete masonry partition walls, where joints occur in concrete floors, and at intersections of masonry walls. A mortar bond should not tie intersecting walls together – a steel tie bar is often used for load bearing intersecting walls to provide load transfer and provide stability without restraining the walls from moving. If the intersecting wall is a non-load bearing partition, galvanized hardware cloth will do the job and is generally placed in every other mortar course.

METHODS ON CONSTRUCTING CONTROL JOINTS

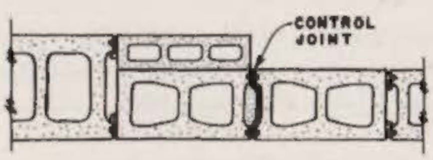
One popular method of constructing a control joint is by using a control joint block. These 8 x 8 x 16 units are used alternately with 8 x 8 x 8 units in the appropriate course to make the control joint. The joint is caulked with an elastic caulking compound.



The control joint shown provides excellent lateral stability to the wall.

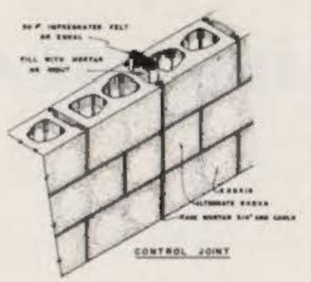
Before placing the caulking compound in a c-joint, the joint should be primed with a sealing material to prevent the dry block from absorbing oils from the caulking compound.

These are examples of instances where control joints are used and the methods of joint construction.



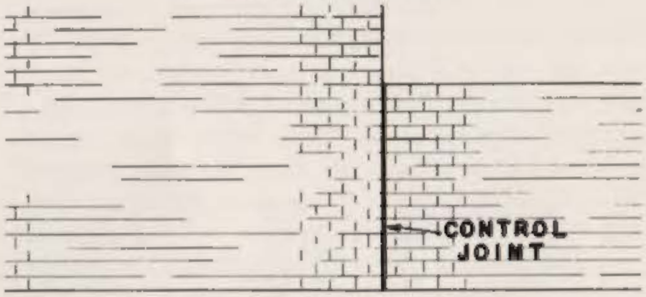
CHANGE IN WALL THICKNESS

Another method of forming a control joint makes use of regular open end units. A strip of 30-pound felt or equal is curled in the core formed by the two ends of the regular open end units placed together, and the core is filled with mortar or grout. These exposed mortar joints are raked ¾″ and caulked with an elastic caulking compound.

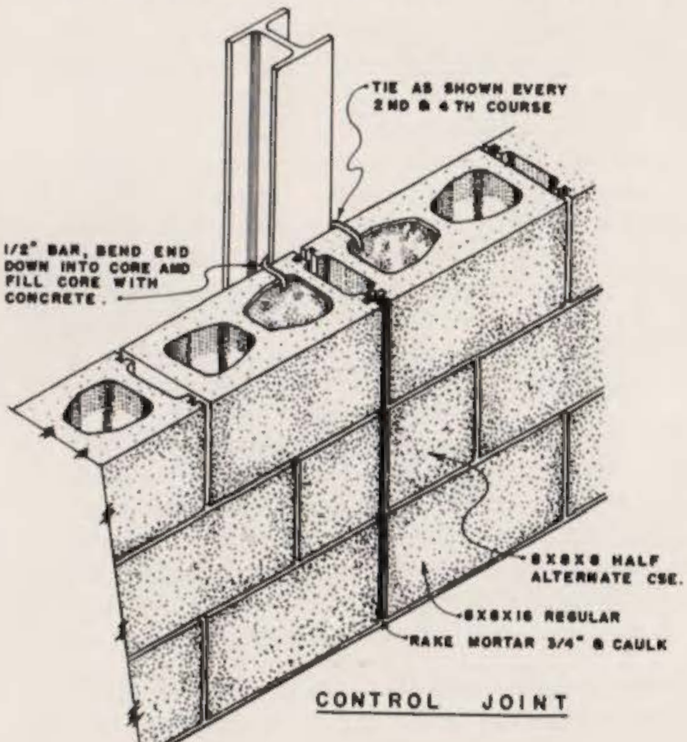


The felt prevents bond, and the control joint allows for small longitudinal movements in the wall.

Please turn to Page 25



CHANGE IN WALL HEIGHT



ILLUSTRATING RECOMMENDED MAX. 20' SPACING OF CONTROL JOINTS

RECOMMENDED LOCATIONS FOR CONTROL JOINTS

manufacture and experimentation

Techniques For Concrete Masonry

BY SAM DIXON, A.I.A.
Housing & Products Engineer
Portland Cement Association
Austin, Texas

The advent of new vibratory types of block machine caused the industry to investigate mixes, curing, handling, and storage methods. One study was an investigation of aggregate types for concrete masonry manufacture. Studies were made of natural aggregate of volcanic origin—commonly called scoria. These are natural deposits of vitrified stone with many small air pockets or cells closely dispersed throughout the material. This excellent aggregate in turn brought about the use of manufactured lightweight aggregates or expanded shale aggregates. Shale, slates and clays having suitable characteristics are kilned at temperatures of from 1900° to 2200°F. Gases formed, usually CO^2, within the shale thus expand, forming myriads of tiny air cells within the mass, which are retained upon cooling and solidification. This results in a cellular aggregate with each cell being surrounded by a hard vitreous membrane. Continued investigation and experimentation is being done in this field.

One of the natural or chemical reactions that takes place when cement and water are mixed is called hydration. This process of hydration continues over a long period of time and this action of water and cement must be kept going in order to develop the qualities we look for in concrete or concrete products. Therefore, we have the process called curing.

Originally, concrete masonry units were—and some still are—cured in air. In order that hydration can be completed the units must be dampened for a period of at least seven days and then stored under cover for a total of at least 28 days so that the required strength and dryness may be obtained. This necessitates a large covered storage yard before a producer can deliver a stable, quality product that meets ASTM specifications.

In order to accelerate the rate of hydration and allow handling sooner, investigations revealed that low pressure steam which is saturated steam curing at atmospheric pressure offered advantages. The units are placed in a room and subjected to steam at 90°-130°F for 12 to 15 hours. This curing method accelerated the rate of hardening of the concrete masonry unit and they could be stock piled in the yard.

The use of low pressure steam brought on high pressure steam curing, commonly called the "Autoclave" process. It results in concrete masonry units ready for use within 24 hours of molding. The compressive strengths of the units at one day are comparable to those of an air water cured unit at 28 days. The units are lighter in color and are much drier because with the rapid release of pressure from the high pressure vessel, a great deal of the moisture in the units is pulled out from the inside toward the outside. The heat and pressure tend to stabilize any unsound materials present that might cause spalling or popping of the unit after it is in service. Investigation also revealed that the substitution of finely ground silica sand for up to 40% of the cement used would result through chemical reactions a more dense and stable unit—one least likely to shrink in service—while retaining the color, texture, and lightness of the product. Autoclaving also eliminated most leaching and efflorescense and increased the units resistance to sulphate action.

It was noted that block stored or used in heavily wooded areas become harder and more stable sooner than did air-water cured block. It was finally traced to the high concentration of CO^2 in these areas. Investigation showed that CO^2 curing had been used in sandlime brick making in Europe since around the turn of the century. Along with hydration, cement carbonization is an action that takes place in curing cement products. Cement is by technical standard 61.5% lime. The so-called free lime or calcium hydroxide released when water is added to cement resulted in compounds that were unstable and which have detrimental effects on concrete. However, the combination of carbon dioxide with this free lime results in calcium carbonate and free water. This is a highly stable combination which reduces a shrinkage tendencies of concrete enhancing the quality which chemically stabilizes it against volume changes. The units are first steam cured at atmospheric pressure for at least eight hours and then CO^2 is introduced into the same kiln or room and allowed to circulate around the units. The results are as described before and are beneficial both in hardness and in strength. Continued investigations are being conducted on this method of curing with apparently promising results.

Strength of concrete masonry walls has been investigated. The Portland Cement Association just recently published a paper "Load Tests of Patterned Concrete Masonry Walls." Most building codes require the wall to withstand a maximum load of 85 pounds per square inch over the gross area. The weakest wall under test resulted in a factor of safety of 4.2 over the required wall strength. The tests were made on load bearing values, so applied to approximate walls in service and transverse loads. Walls of many patterns were tested including running bond, basket weaves, and coursed ashlar. Walls with continuous vertical joints were about 30% weaker than those of running bond. The diagonal basket weaves and diagonal bonds failed due to mortar shear or loss of bond between unit and mortar. However, the weakest wall was well within the code requirements and had a factor of safety of 4.2.

Another field of study has been in the glazed plastic face block. Recently a company has come out with an improved sand called S.G. sand. With this in their facing mix, these units will meet all the requirements of ASTM C-126 set up for glazed structural clay products. Tests are available from independent testing labs from various parts of the states that indicate complete compliance with ASTM C-126 specifications. This faced unit is impervious, meets the opacity requirements, resists the listed chemicals, is resistant to crazing and staining, will not support combustion and has a "fire factor" of 28.2. This is very good when you compare it to the 75 allowable maximum for materials in corridors of public buildings. About 1/3 that allowed by the most stringent codes.

Studies are underway dealing with the use of heavy aggregates and thicker face shells for use in low order nuclear shielding. These units will have a unit weight of 150 pounds per cubic foot. Experimentation in this field looks very promising. These units use barites, dolomites, traprock, limonites, magnetite and steel, or iron punchings as aggregates. Saving in time and labor can be made if low order radiation shielding is needed in existing plants of hospitals and laboratories if you could design and build these shields of concrete masonry units and not have to go into extensive remodeling or demolitions in order to construct such shielding.

Then there are new shapes in concrete masonry units. These coupled with white marble aggregates, white sands, and white cement and, of course, covering compounds and portland cement paints leave no limit on the designer. The shapes and forms of his ideas are only limited to his own ingenuity as a designer. They are practically unlimited in scope—these new shapes.

Finally frets are being applied to concrete masonry units and fired up to 2300°F to make porcelainized faces. Much work is being done in this field of study in order to get colors and glazed impervious faces on the units.

These, then, are some of the ideas and techniques that have been advanced in this industry. There are many more under consideration and test. When more information is available, it will be passed on to you.

designing concrete masonry WALLS

BY W. E. KUYKENDALL, A.I.A.
El Paso, Texas

Assuming good engineering practices are followed in the preparation of soil base and the design of footings, the architect's first consideration in the design of concrete masonry walls is the utility and function of the structure. Secondly, he must consider its esthetic value as related to the whole. Finally, and of no small significance, is the soundness of structure and its ability to withstand the ravages of time, elements, and children.

The basic requirements having been established, proper attention to detail now becomes a factor. Overall length and height of walls, openings and returns should be carefully planned to utilize stock shapes and sizes of masonry units, thereby eliminating the need for costly and unnecessary cutting and filling. Careful selection of modular doors and windows is of prime importance. A wall laid out in four inch modules will assure the architect of an orderly and economical assembly.

Concrete masonry units, as all masonry materials, are subject to expansion and contraction when exposed to moisture and temperature changes. To compensate for this movement, control joints should be located at openings, changes in wall heights, and at recommended distances in long, unbroken walls. Changes in wall heights may also be treated with a bond beam running in and completely around the top course of the lower wall, or up to a point where a control joint is reached.

Having laid out the walls and located control joints, next comes the design of bond beams and placement of joint reinforcing. Such requirements will often vary according to the individual application, but, in general, masonry reinforcing should be placed on sixteen inch centers vertically, and bond beams should occur at eight foot intervals in the height of the wall.

Good bonding of concrete masonry units requires good mortar. In the design of a mortar mix, proportioning of materials will be dependent on strength criteria and the degree of exposure. A good rule-of-thumb, however, for a mortar to be used above-grade, is one part Portland Cement, one part hydrated lime or lime putty, and six parts clean, sharp sand. For applications below grade or in columns and footings, use a mix containing one part Portland Cement, one-fourth part lime or lime putty, and two or three parts sand.

The final and most important step in the procedure is masonry erection. The masonry contractor must take care to assure that all units are laid plumb and true, that all head and bed joints are sufficiently tight and properly aligned, and that joint tooling is done at the most appropriate time. He must also see that no unit is moved after being placed in mortar, for any movement at this time will surely impair the bond and lead to future problems.

Joint types preferred are the Concave, the Vee, and the Weathered joints. Good tooling practice where the mason can shove the mortar tight against the edges of both units will result in weathertight joints, and weathertight joints make weathertight walls.

There are innumerable methods for finishing and decorating concrete masonry walls. These, of course, will vary depending on the desired result.

All too often the painter is called upon to perform extra duty in concealing errors made by the mason. Concrete masonry walls—or any walls—are and can be no better than the quality of materials and workmanship used in their assembly . . . and some errors even Michaelangelo couldn't hide. Be sure of good working plans. Be sure of quality materials. Select a qualified and proven masonry contractor. Remember—"you get what you pay for."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Architectural Design

in concrete masonry

BY CHARLES M. MCKIM, A.I.A.
Houston

In recent years the use of highly decorative elements has again crept into Architectural design. With the use of these decorative elements the designer's "search for expression" has become a search for materials with which to express himself. With its myriad possibilities, concrete masonry has become an impressive factor in this search. Concrete masonry of today offers characteristics not found collectively in any other material. It provides excellent sound absorption qualities and insulating values, is highly fire resistance, and has excellent structural qualities. Its use is certainly not prohibitive in cost, and minimum maintenance makes it even more desirable.

The versatility by which concrete masonry caters to the designers' needs is amazing. There are an unlimited number of surface finishes and textures to be obtained by an ever-increasing supply of new materials. Surface textures and colors may be changed as easily as changing the aggregate in the units. Complete wall surface textures, or patterns in light and shadow, may be obtained by simply arranging the units themselves into the desired position. Grilles, using either standard or special shapes, are appearing in never ending combinations. Friezes and accents are encountered in many designs. Ceramic tile, glass, brick, metals and many other materials used in combination with concrete masonry units seem to enhance both materials and only add to the unlimited uses to which concrete masonry may be put.

Concrete masonry, thanks to the imaginative designers and progressive manufacturers of today, has turned into one of the most interesting and flexible materials at our command.


THE
FEATHERLITE BLOCK CO.
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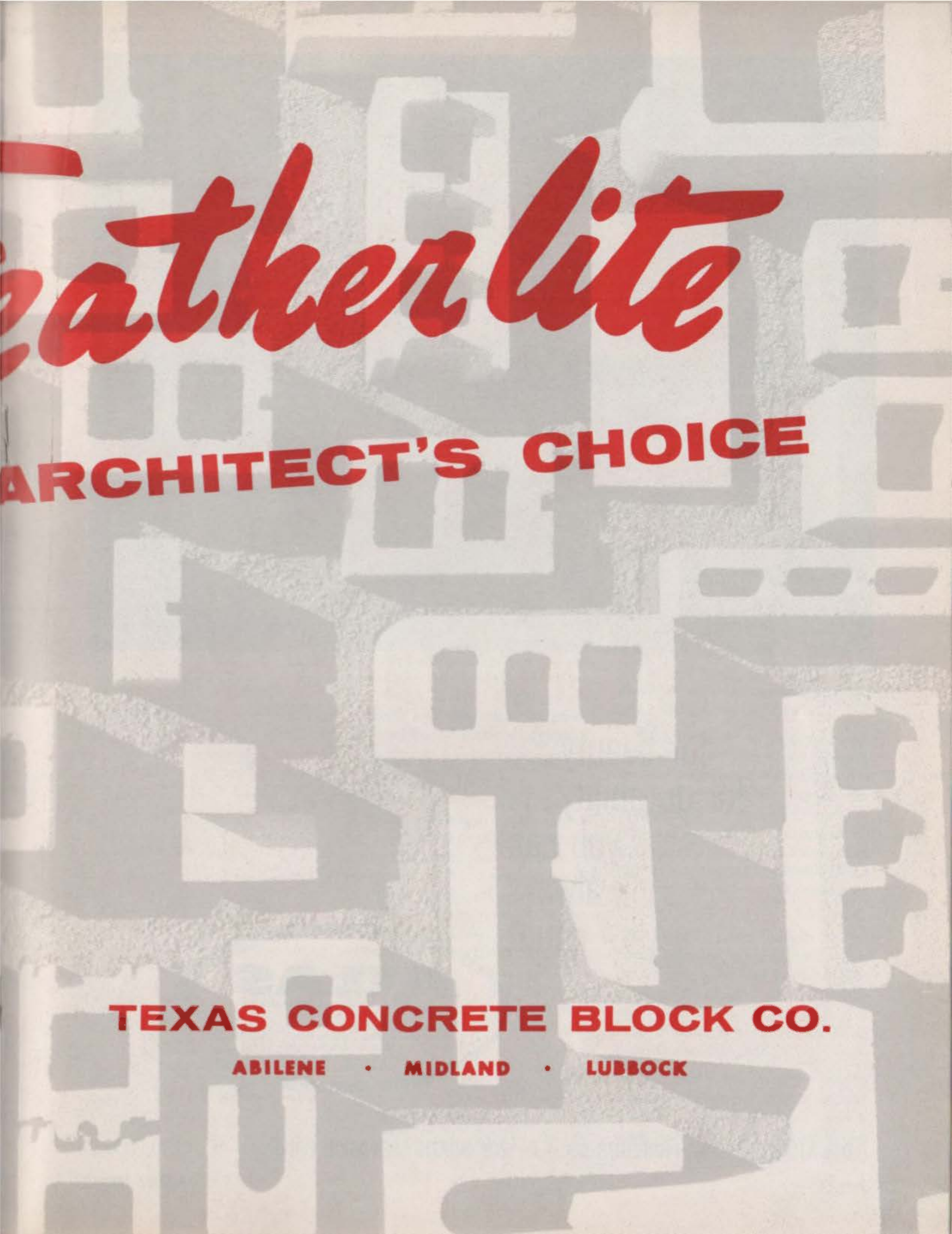
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CRACK-FREE

cement plaster jobs

A new method of preventing cracks in Portland cement plaster jobs while retaining strength and durability is considered an unqualified success by Texas architects who have proven its merit on a variety of building projects over the past year.

Without exception, the reports have uniformly been: "No drying cracks," even in situations where a severe cracking tendency was known to exist. As a result, it is anticipated that the use of Portland cement plaster may double or even triple.

The key to the improved method is a spreading and plasticizing agent named X-59 by its originators, James E. Madden and W. J. Newell of Fort Worth. Only three-quarters of a pound of X-59 per sack of cement, plus sand and water produces a plaster which may be applied with ease but which keeps unchanged the strength and shrinkage properties characteristic of Portland cement.

Madden's search for the right material stemmed from forty years in the plastering trade, observing how available spreading agents reduced the strength and increased the shrinkage so that costly touch-up work was often required. He found the answer in a finely divided silica produced by the Cabot Corporation of Boston, Massachusetts. Laboratory tests confirmed field observations that, in the proportion of ¾ pound of X-59 to a sack of cement, the plaster not only had the same drying shrinkage but also retained the high compressive, flexural and tensile strength of straight Portland cement sand combinations.

Among the earliest architects to take advantage of the material was Edward Wilson of the Fort Worth firm of Wilson, Patterson, Sowden, Dunlap and Epperly, who specified it for several of the North Texas State University buildings in Denton, including the canopy ceiling around one side of the music building. The results were so good that he has specified it for a number of subsequent jobs, including all the cement plaster in the Birdville Baptist Sunday School Building just outside Fort Worth.

"We're very pleased with this material," comments Mr. Wilson. "We've used it repeatedly, and it has been successful with no shrinkage problem."

Similar results in Fort Worth were obtained in nearly a quarter-mile of canopy ceilings for Alcon Laboratories, where the architectural firm was Floore and Hueppelsheuser; and the canopy ceilings of the new Telephone Credit Union, where Woltz and Lane were the architects.

X-59 is available in ten-pound bags through Van Waters and Rogers, Inc., of Houston and Dallas, and a premixed product is planned for availability in six months to meet anticipated demand. The excellent results secured by users have more than justified the cost of the X-59, which is about 75¢ per bag of cement in the plaster mix.

The X-59 is added directly to the mixer with the other ingredients at the time each batch of Portland plaster is prepared, and contractors using it have found that the preferable order of addition is water, then X-59, then cement, then sand.

Mixing specifications for the scratch coat include one bag of Portland cement, ¾ pound X-59, 2 to 2½ cubic feet of sand over the metal lath base, or 2 to 3 cubic feet of sand over masonry base. For the brown coat, the mix is one bag of Portland cement and ¾ pound of X-59 to a minimum of 3 cubic feet of sand. For a sand finish, interior or exterior, the finish coat mix is one bag of Portland cement and ¾ pound of X-59 to 2 to 2½ cubic feet of sand. For the finish coat only, added workability may be obtained by adding finishing lime in an amount not to exceed 10 percent of the weight of cement used.

The X-59 plaster pumps readily to different levels of the job and applies very satisfactorily by machine.

The basic material of X-59 is a grade of pyrogenic collodial silica, whose special properties have previously found useful application as a reinforcing agent in silicone rubber, a suspending agent in paints, a flatting agent in varnishes and lacquers, and a free-flowing or anti-caking agent. Its new utilization in the building field solves a long-standing problem for architects and plaster contractors.

Continued from Page 13

In discussing the use of horizontal wire reinforcement, it is best to say that horizontal reinforcement does not eliminate cracking in masonry walls; it merely controls cracking. Reinforcement does nothing until the wall begins to crack. At this time, the higher tensile steel wire pulls against the lower tensile mortar joint, or masonry unit, and tends to close the crack or keep the crack very small.

When a crack occurs in an un-reinforced masonry wall, the crack becomes a weak point, and further cracking may occur at this point, resulting in a larger crack. In a reinforced wall, there may be fine hairline cracks that are barely visible in most instances.

The size of cracks and the effectiveness of the horizontal reinforcement to do its job is largely dependent upon the bond strength that can be developed between the reinforcement and the masonry mortar. The better the bond strength, the quicker the wire reinforcement acts against cracking.

Experience has shown that cracks in masonry walls tend to be localized in certain areas, areas of stress concentrations such as windows, doors and parapet walls. A good rule to follow is to require that the first two courses above and below all wall openings be reinforced. Reinforcement above and below openings should extend at least 24" beyond the openings. The use of horizontal reinforcement in the balance of the wall should be dependent upon the length of the wall, spacing of control joints or wall design. Horizontal reinforcing should not be placed through a control joint.

When placing horizontal joint reinforcing in a wall, the mortar should be spread first and the reinforcing placed in the mortar, rather than reinforcing and then mortar. This method gives a better bond strength and a greater resistance to corrosion.

It is wise to use the right thickness of side rods for the mortar joint, generally a reinforcement which equals one-half the thickness of the mortar joint. Using a side rod too heavy for the joint may actually cause the wall to crack because the rod is unprotected by mortar and may rust. The rusting of the unprotected rod may cause expansion and a crack may occur. The problem of insufficient bonding occurs when using reinforcing which is too thick—then it will not develop its reinforcing potential.

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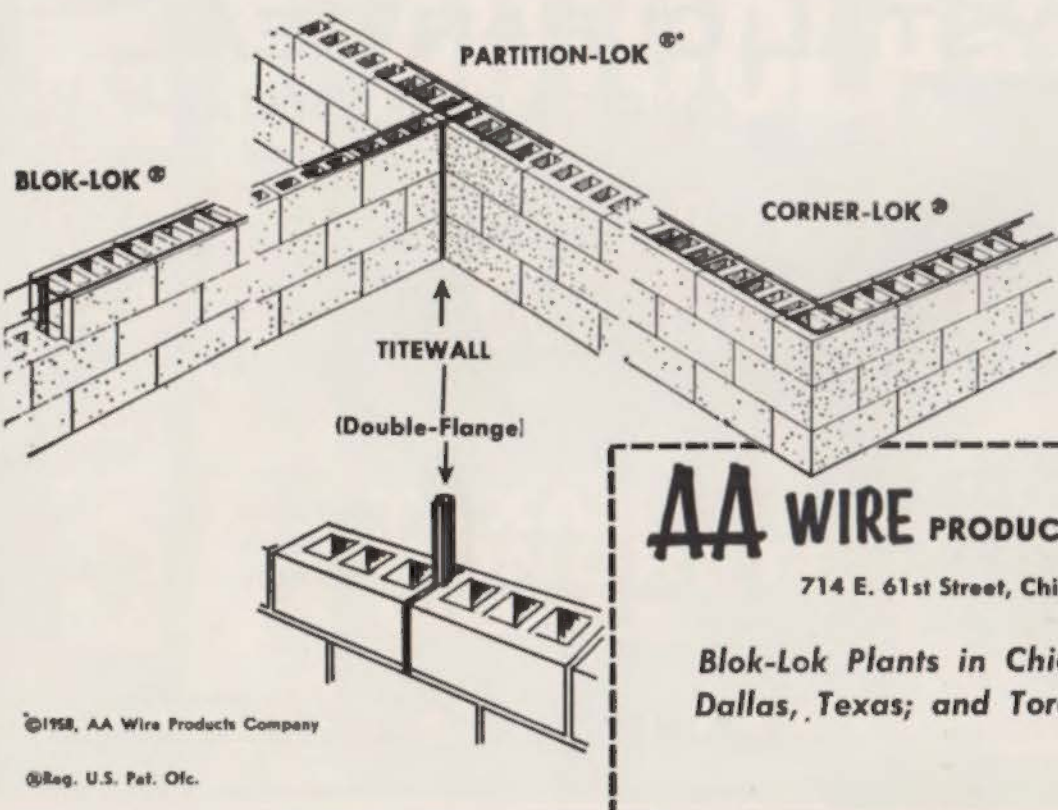
For maximum bond strength and maximum corrosion resistance, lay BLOK-LOK in mortar bed as shown above. Only steel in tension adds strength.



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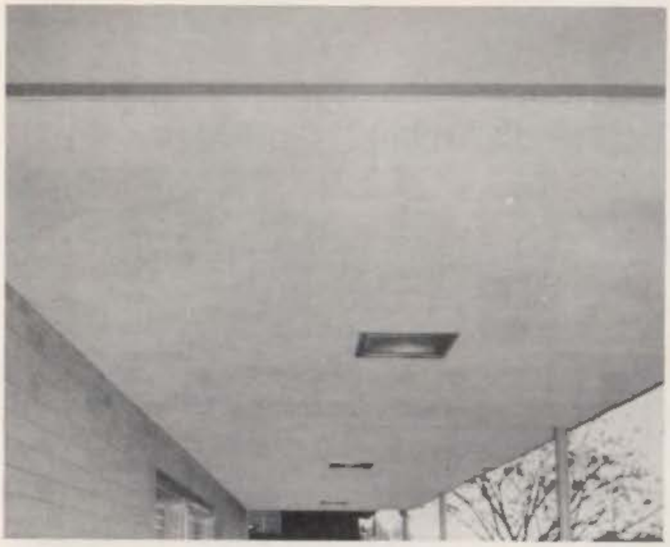

completely free from cracks

Typical of Portland cement plaster work using Texas-originated X-59 is the close-up of canopy ceiling at left, after months of test exposure. Regarding the X-59 use in the H. S. Thompson School of Dallas, at right, architect J. Allen Boyle of Dallas says: "This suspended plaster ceiling of more than 14,000 square feet was installed during the very hottest and driest Texas July-August days—a true test for any material."

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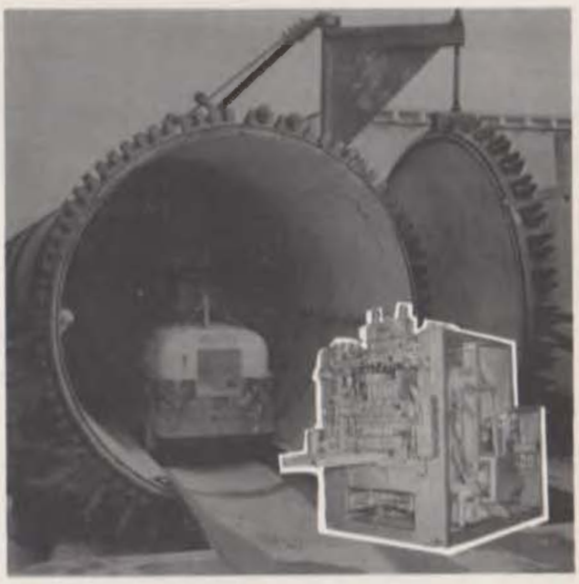

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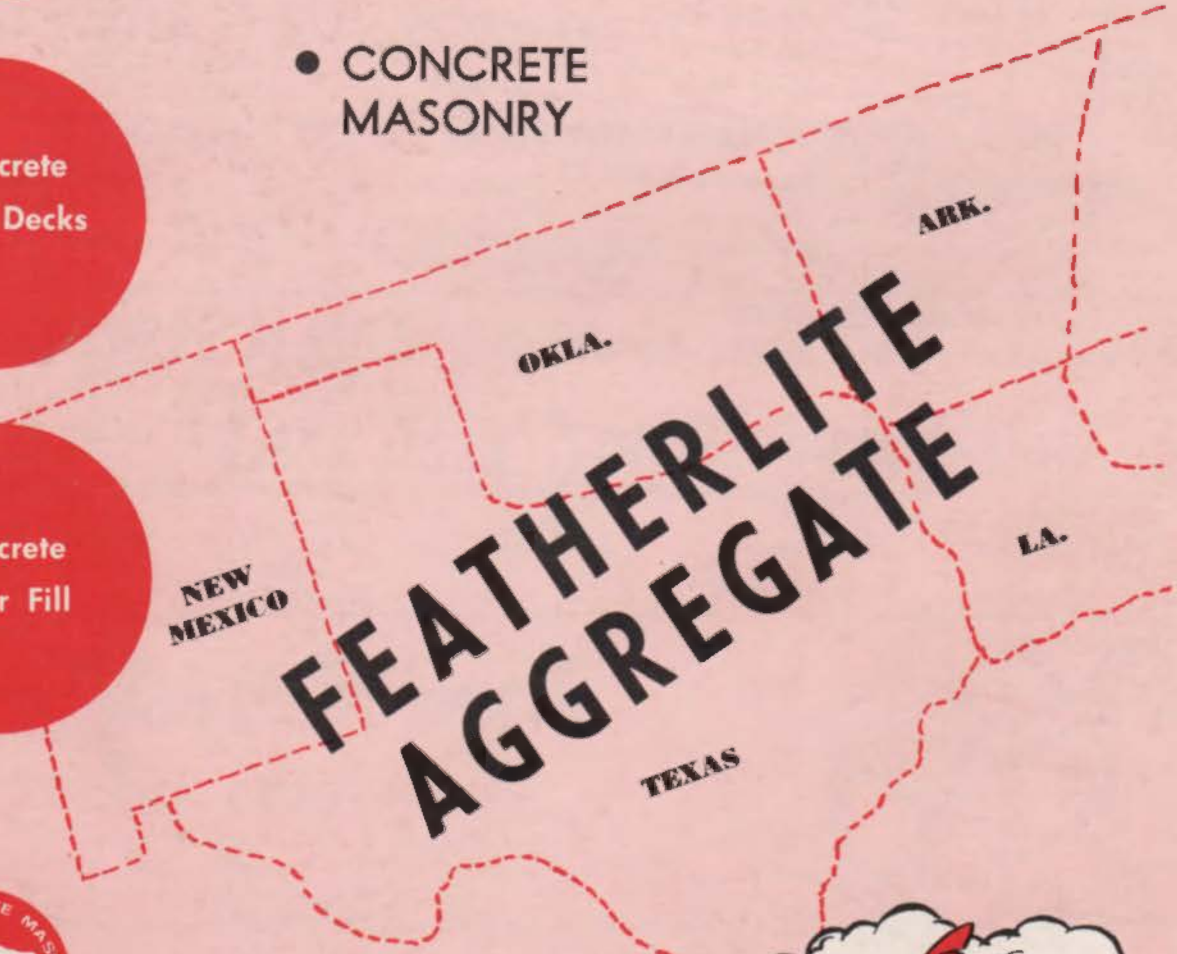

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